

Centrifugation - Goals for this unit:

1. Understand essential theoretical concepts of movement of a particle under a centrifugal force. $F_s + F_b + F_f = 0$

2. Know differences between "preparative" and "analytical" types of centrifugation. RCF = Relative Centrifugal Force

3. Analytical Centrifugation

Instrument

Optic systems - general principles / how to interpret them

Schlieren / Interference / Absorption optics

Common Applications (transport vs. equilibrium experiments)

Sedimentation Coefficient - "s" vs. "S"

Diffusion Coefficient $D = RT/Nf$

Frictional Coefficient / frictional coeff. ratio $f = 6\pi\eta R$

Sedimentation Equilibrium

Sedimentation of Particles in a Gravitational Field

constant velocity = u

$F_f = -fu$

$F_b = -m_0\omega^2 r$

$F_s = m\omega^2 r = \frac{M}{N}\omega^2 r$

$m_0 = m\bar{v}\rho = \frac{M}{N}\bar{v}\rho$

$F_s + F_b + F_f = 0$

$\frac{M}{N}\omega^2 r - \frac{M}{N}\bar{v}\rho\omega^2 r - fu = 0$

$\frac{M}{N}(1 - \bar{v}\rho)\omega^2 r - fu = 0$

$\frac{M(1 - \bar{v}\rho)}{Nf} = \frac{u}{\omega^2 r} \equiv s$

Table 1. Approximate Values of Partial Specific Volumes for Common Biological Macromolecules

Substance	\bar{v} (mL/g)	
Proteins	0.73	(0.70-0.75)
Polysaccharides	0.61	(0.59-0.65)
RNA	0.53	(0.47-0.55)
DNA	0.58	(0.55-0.59)

Data from Beckman review article by Greg Ralston.

Preparative Centrifugation

1. Principles of Centrifugation / theory and key equations

$$F_s = m\omega^2 r = \frac{M}{N}\omega^2 r$$

where ω = angular velocity (radians / sec)

r = radius of particle from axis of rotation

note: ω (1/sec) = rpm x (2 π rad / rev) x (1 min / 60 sec)

$$\text{RCF (Rel. Centrifugal Force)} = \frac{F_c}{F_g} = \frac{m\omega^2 r}{ma} = \frac{(2\pi \text{ rpm}/60)^2 \times r}{980 \text{ cm/ sec}^2} = 1.119 \times 10^{-5} (\text{rpm})^2 r$$

for $r = 9.0$ cm

rpm	1000	5000	10,000	20,000	40,000
RCF	100	2500	10,000	40,000	160,000

Use of Centrifugation in Biochemistry

$$\frac{M(1 - \bar{v}\rho)}{Nf} = \frac{u}{\omega^2 r} \equiv s$$

1. Preparative Centrifugation

- rotors
- density gradient methods
 - sucrose gradients / isopycnic methods (CsCl gradients)

2. Analytical Ultracentrifugation

- instrument and optic systems
- sedimentation velocity experiments
 - sed. coefficient (s) ($S = 10^{-13}s$)
- sedimentation equilibrium exp.
 - molecular weight
- diffusion constants /

$$D = \frac{RT}{Nf}$$

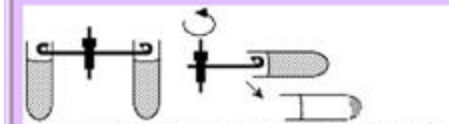
Centrifuge Rotors

A. Fixed Angle Rotor



Advantage: Sedimenting particles have only short distance to travel before pelleting. **Shorter run time.** The most widely used rotor type.

B. Swinging Bucket Rotor

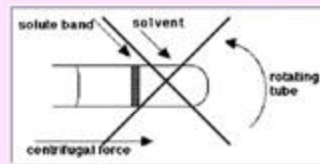


Advantage: Longer distance of travel may allow better separation, eg in density gradient centrifugation. Easier to withdraw supernatant without disturbing pellet.

<http://www.resonance-pub.com/centrifuge.htm>

10.4 Density Gradient Centrifugation

In absence of a density gradient, separated bands of solute in the centrifuge are gravitationally unstable.



CANT OCCUR because layer of concentrated, dense solution overlaying less dense solvent would lead to mixing by convection and muddle the separation. In absence of stabilising density gradient, cat form boundaries (cf electrophoresis 9.3) but not zones. In analytical ultracentrifuge, moving boundaries and concentration distributions observed by optical device.

Create DENSITY GRADIENT in tube

Use a non-interacting, low MW solute in continuously increasing concentration from meniscus to bottom of tube.

Important technique for purifying proteins and particularly nucleic acids.

Two different types of density gradient centrifugation, for two different purposes are:

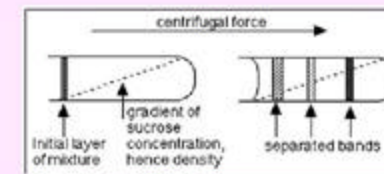
- Zonal (or Rate Zonal) Centrifugation (sucrose density gradient centrifugation)
- Isopycnic Centrifugation (Cesium chloride density gradient centrifugation)

<http://www.resonance-pub.com/centrifuge.htm>

Zonal Centrifugation

<http://www.resonance-pub.com/centrifuge.htm>

Mixture to be separated is layered on top of a SUCROSE, or FICOLL, GRADIENT (increasing concentration down the tube) - provides gravitational stability as different species move down tube at different rates forming separate bands.



Species are separated by differences in SEDIMENTATION COEFFICIENT (S)

$$= \frac{\text{Rate of movement down tube}}{\text{Centrifugal force}}$$

S is increased for particle of LARGER MASS (because sedimenting force $\propto M(1-\bar{v}\rho)$)

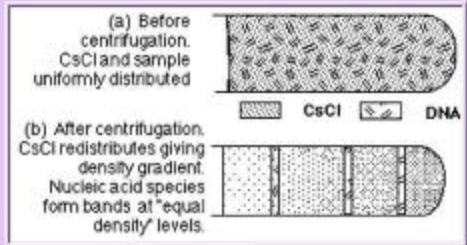
S is also increased for MORE COMPACT STRUCTURES of equal particle mass (frictional coefficient is less)

Mild, non-denaturing procedure, useful for protein purification, and for intact cells and organelles.

Isopycnic Centrifugation

Molecules separated on EQUILIBRIUM POSITION, NOT by RATES of sedimentation. Each molecule floats or sinks to position where density equals density of CsCl solution. Then no net sedimenting force on molecules.

Isopycnic = Equal density
and separation is on basis of DIFFERENT DENSITIES of the particles.



(a) Before centrifugation. CsCl and sample uniformly distributed

(b) After centrifugation. CsCl redistributes giving density gradient. Nucleic acid species form bands at "equal density" levels.

Very useful for purifying nucleic acid species of different density, also in separating proteoglycans extracted from cartilage.

<http://www.resonance-pub.com/centrifuge.htm>

Analytical Ultracentrifuge:
The sorts of questions for which answers are sought

- (1) Is the sample homogeneous? Is it pure?
- (2) If there is a single component, what is the molecular weight?
- (3) If more than one type present, can the molecular weight distribution of the sample be obtained?
- (4) Can an estimate be obtained of the size and shape of the particles? Are the molecules compact and spherical (globular) or long and thin (rod-like)?
- (5) Can the macromolecules be distinguished on the basis of density?
- (6) Can interactions between solute molecules be detected? Aggregation between molecules changes molecular weight, changes in molecular weight as a function of the concentrations of the components can illuminate the type of reaction (e.g., reversible or nonreversible?), the stoichiometry, and the strength of binding.
- (7) Can changes in conformation or shape of the particles be measured?

Molecular Weight Determination

Light scattering / Centrifugation / Osmometry / X-ray diffraction / Mass Spec

Electrophoresis and chromatographic methods are popular for rapid estimation of molecular weights of proteins and nucleic acids. However, such methods, though rapid and sensitive, have **no rigorous theoretical base; they are empirical techniques** that **require calibration and assumptions** that may be invalid.

The **analytical ultracentrifuge** enables the **direct measurement of molecular weights** of solutes in the **native state** and as they exist in solution, **without calibrations or assumptions concerning shape**. The method is applicable to molecules with molecular weights ranging from several hundreds (sucrose) up to many millions (virus particles).

Sedimentation equilibrium methods require only **small sample sizes (20-120 μ L)** and **low concentrations (0.01-1 g/L)**.

Conformational Changes

X-ray diffraction and **NMR techniques** are currently the only techniques available that are capable of providing structural details at **atomic resolution**.

Nevertheless, **the overall size and shape of a macromolecule or complex in solution can be obtained through measurement of the rate of movement of the particles through the solution**. Sedimentation velocity experiments in the analytical ultracentrifuge provide **sedimentation and diffusion coefficients** that contain information concerning the **size and shape** of macromolecules and the interactions between them. Sedimentation coefficients are particularly useful for monitoring **changes** in conformation in proteins.

Use of Centrifugation in Biochemistry

$$\frac{M(1 - \bar{v}\rho)}{Nf} = \frac{u}{\omega^2 r} \equiv s$$

1. Preparative Centrifugation

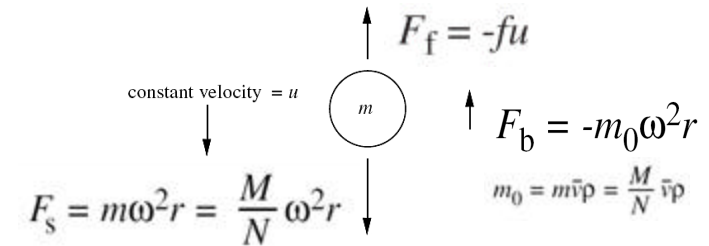
- rotors
- density gradient methods
sucrose gradients / isopycnic methods (CsCl gradients)

2. Analytical Ultracentrifugation

- instrument and **optic systems**
- **sedimentation velocity** experiments
sed. coefficient (s) ($S = 10^{-13}s$)
- **sedimentation equilibrium** exp.
molecular weight
- **diffusion constants** /

$$D = \frac{RT}{Nf}$$

Sedimentation of Particles in a Gravitational Field



$$\frac{M(1 - \bar{v}\rho)}{Nf} = \frac{u}{\omega^2 r} \equiv s$$

$$D = \frac{RT}{Nf}$$

$$M = \frac{s^0 RT}{D^0(1 - \bar{v}\rho)}$$

Centrifugation: Terms and Units

Force: mass x acceleration ($F = ma = m\omega r^2$)
(g cm / sec²)

Energy: force x distance Joule = Kg m²/ sec²
erg = g cm²/ sec²

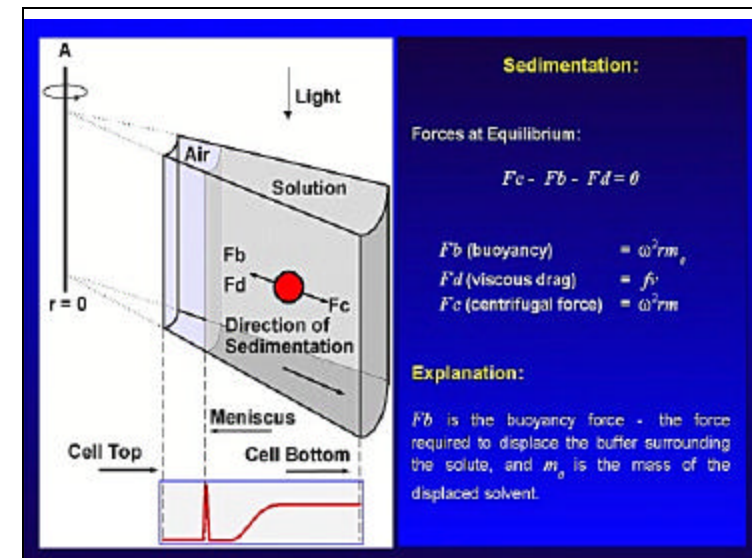
Partial specific volume \bar{v} (cm³/g)

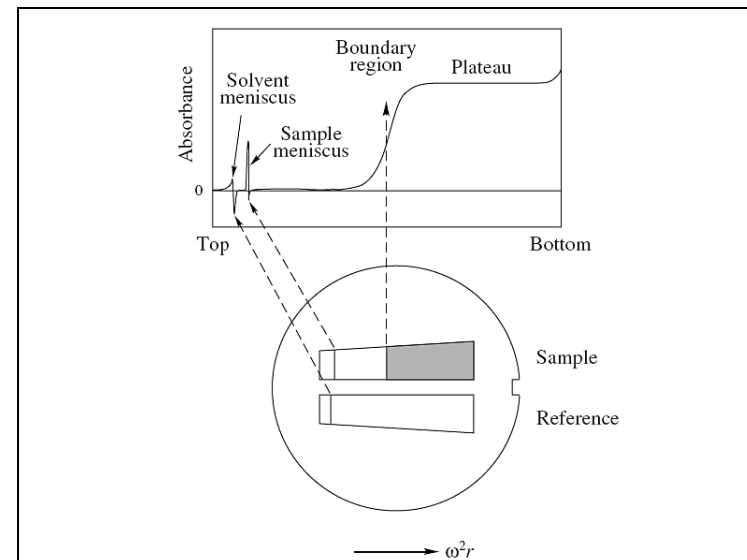
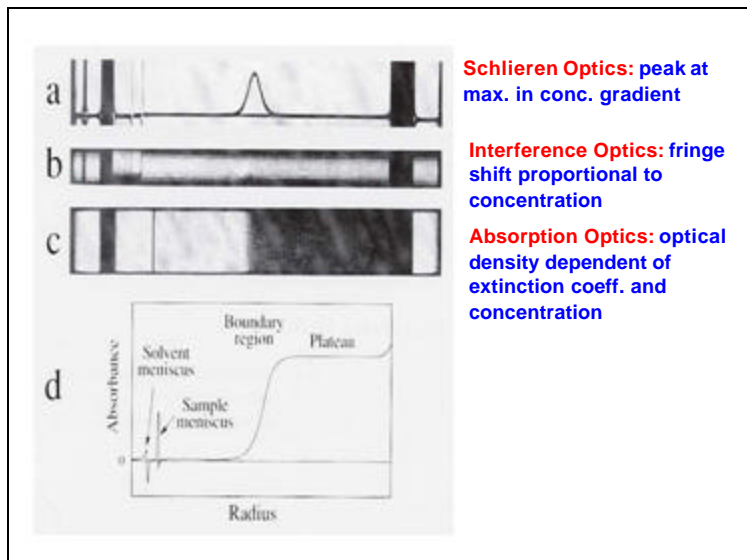
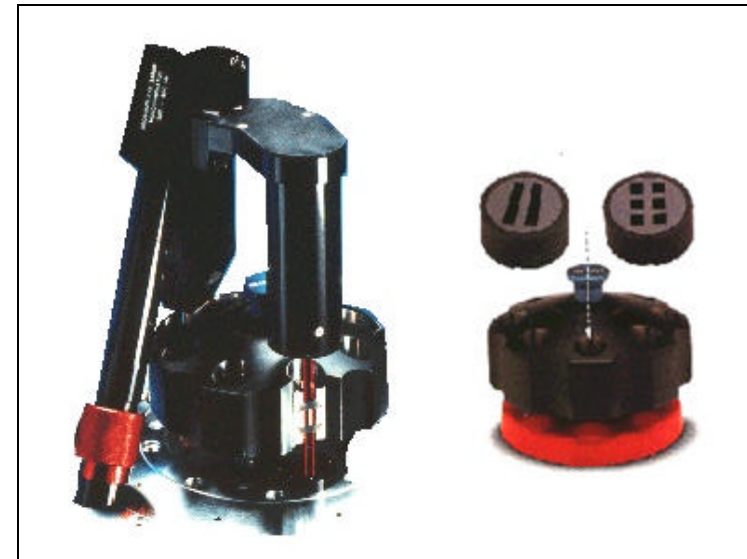
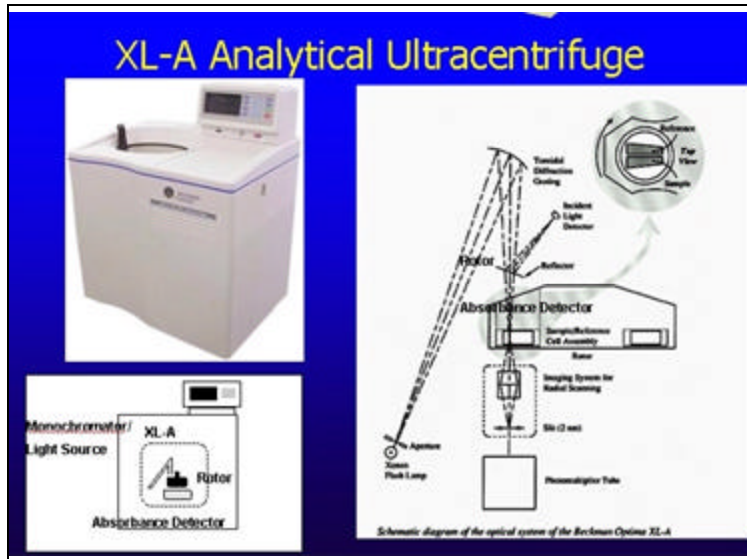
Viscosity: η (~0.01 g/(cm-sec))

Frictional Coefficient: $f = 6\pi\eta R_0$ (~10⁻⁸ g/sec)

Sedimentation Coefficient: s (sec) [1S = 10⁻¹³ s]

Diffusion Constant: $D = \frac{RT}{Nf}$ (cm²/s)





II. Interference Optics ($\Delta J \approx \Delta c$)

Count along this line $Y = Y_0$ 0 1 2 3 4 5 6 7 8 Y_v Y_f
 Fractional Fringe = $\frac{Y_f}{Y_v}$

shifting fringes

$\Delta J = \frac{a}{\lambda} \Delta c = \frac{a}{\lambda} \left(\frac{dn}{dc} \right) \Delta c$ or $\Delta c = \frac{\Delta J \cdot \lambda}{a \cdot K}$

$\Delta c = \frac{\Delta J \cdot \lambda}{a \cdot K}$ **DJ from fringes**

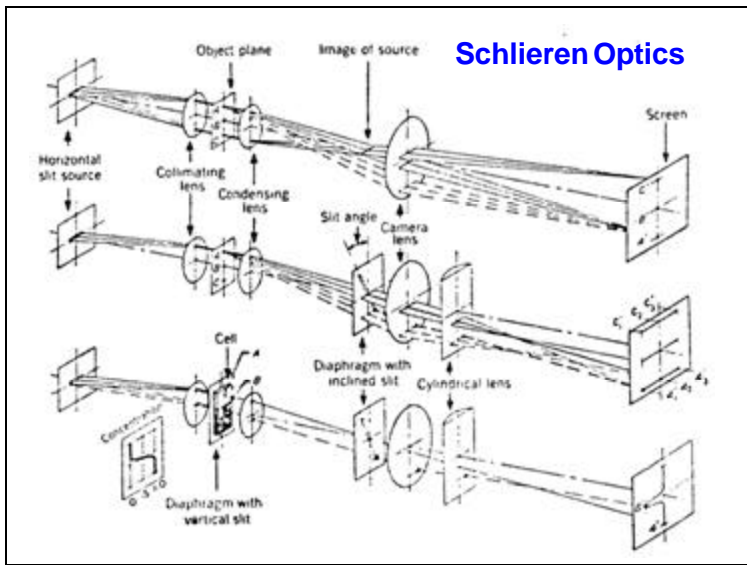
$\frac{dn}{dc} = K = 0.186 \text{ (g/cm}^3\text{)}^{-1}$; $a = 12 \text{ mm}$; $l = 546 \text{ nm}$

Count along this line $Y = Y_0$ 0 1 2 3 4 5 6 7 8 Y_v Y_f
 Fractional Fringe = $\frac{Y_f}{Y_v}$

$\Delta c = \frac{\Delta J \cdot \lambda}{a \cdot K}$

where $DJ = h / d$
 $a = 12 \text{ mm}$; $l = 546 \text{ nm}$
 $\frac{dn}{dc} = K = 0.186 \text{ (g/cm}^3\text{)}$

Since $c = c_m + Dc$
 $c \sim Dc$
 when $c_m \sim 0$ (Yphantis high speed condition)



I. Schlieren Optics ($\alpha \propto \frac{dc}{dx}$)

$n \approx n_0 + \frac{dn}{dc} \cdot c$
 $\alpha = a \frac{dn}{dx} = a \frac{dn}{dc} \frac{dc}{dx} = a K \frac{dc}{dx}$

Conventional Cell Double Sector Cell Conventional Cell

How can we measure s in the Ultracentrifuge?

$$\frac{\Delta l (1 - v \rho)}{Nf} = \frac{v}{\omega^2 r} = s$$

Express the velocity in terms of a derivative. $v = \frac{dr}{dt} = \omega^2 r s$

Integrate: $\int_{r_0}^{r_1} \frac{1}{r} dr = \omega^2 s \int_{t_0}^t dt$ $s = \ln\left(\frac{r_1(t)}{r_0(t_0)}\right) [\omega^2 (t - t_0)]^{-1}$

The XLA provides both $\omega^2 \Delta t$ and the radial positions, r

Sedimentation Velocity

$$s \equiv \frac{u}{\omega^2 r} = \frac{dr_{\text{bnd}}/dt}{\omega^2 r}$$

$$\ln(r_{\text{bnd}}/r_m) = s\omega^2 t$$

$$s \equiv \frac{u}{\omega^2 r} = \frac{dr_{\text{bnd}}/dt}{\omega^2 r}$$

$$\ln(r_{\text{bnd}}/r_m) = s\omega^2 t$$

Recall: $s = \frac{v}{\omega^2 r} = \frac{1}{\omega^2} \frac{1}{r} \frac{dr}{dt}$ This is a Differential Equation which we can easily solve by separating the variables and integrating: $\int_{t_0}^t \omega^2 s dt = \int_{r_0}^{r_1} \frac{1}{r} dr \implies \omega^2 s (t - t_0) = \ln \frac{r_1}{r_0}$

We integrate between $t = t_0$ ($r = r_0$) and $t = t$ ($r = r_1$); r_0 is the boundary position at the start ($t = t_0$) and r_1 is the boundary position at later time(s). Thus, if we plot $\ln \frac{r_1}{r_0}$ vs. $(t - t_0)$, the result is a straight line with a slope = $\omega^2 s$.

$$s_{20,w} = s_{\text{obs}} \left(\frac{\eta_{T,w}}{\eta_{20,w}} \right) \left(\frac{\eta_c}{\eta_w} \right) \left(\frac{1 - \bar{v} \rho_{20,w}}{1 - \bar{v} \rho_{T,w}} \right)$$

Figure 1: A single-component system shown without diffusion (in blue) and with diffusion (in red). The boundary spreads due to diffusion and gives a sigmoidal shape to the boundary.

Figure 2: A multi-component system shown without diffusion (in blue) and with diffusion (in red). The step functions defining the boundary profiles of each component can lose definition as diffusion increases and overlays on top of sedimentation separation.

Flow in the Ultracentrifuge Cell:

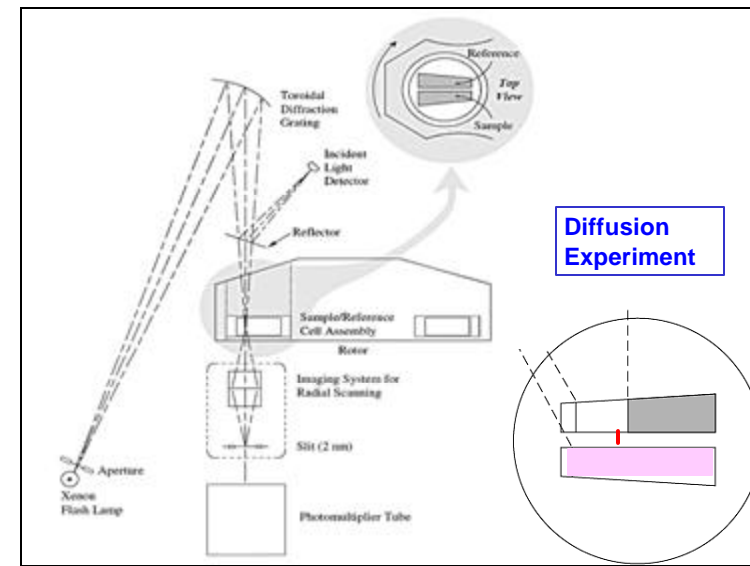
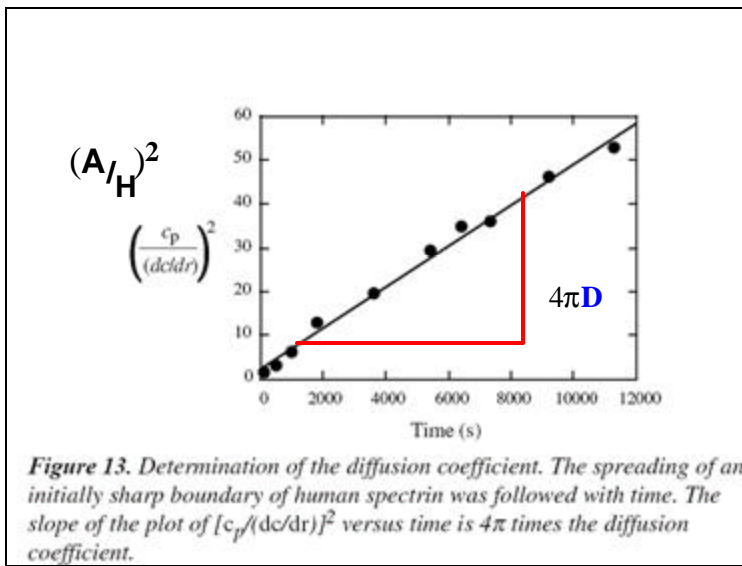
Sedimentation: $\frac{M(1-\bar{v}\rho)}{Nf} = \frac{v}{\omega^2 r} = s$

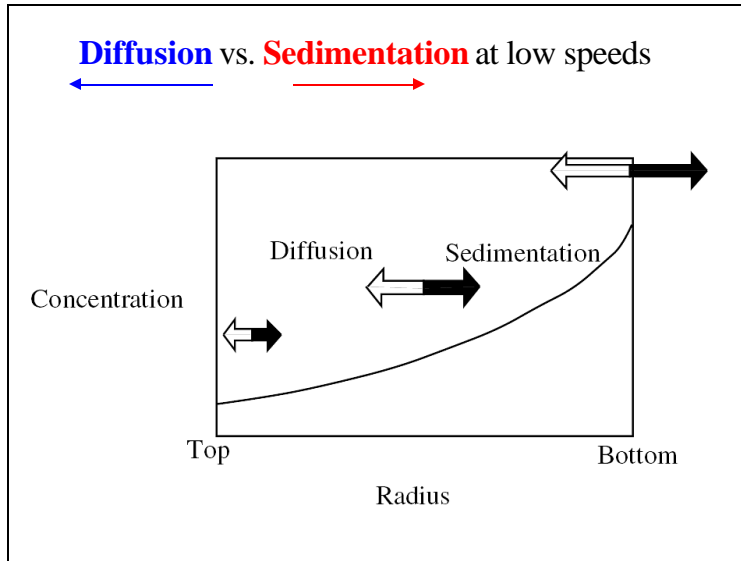
Diffusion: $D = \frac{RT}{Nf}$

Molecular Weight: $\frac{s}{D} = \frac{M(1-\bar{v}\rho)}{RT}$

The ratio of s/D is proportional to the Molecular weight

$$M = \frac{s^0 RT}{D^0(1 - \bar{v}\rho)}$$

$$f = 6\pi\eta R \qquad D = \frac{RT}{Nf}$$




Sedimentation Equilibrium

At Equilibrium, the total flow is zero, and diffusion and sedimentation exactly balance out:

$$J = s\omega^2 r C - D \frac{\partial C}{\partial r} = 0 \quad \text{Therefore:} \quad s\omega^2 r C = D \frac{\partial C}{\partial r}$$

Since: $\frac{s}{D} = \frac{M(1-\bar{v}\rho)}{RT}$

$$\frac{\partial C}{C} = \frac{M\omega^2 r(1-\bar{v}\rho)}{RT} \partial r$$

Sedimentation Equilibrium

$$\int_{c_0}^{c_r} \frac{1}{C} dC = \frac{M\omega^2(1-\bar{v}\rho)}{RT} \int_{r_0}^{r_r} r dr$$

After integration: $C = C_0 \exp \frac{M\omega^2(1-\bar{v}\rho)}{RT} (r^2 - r_0^2) + \text{Baseline}$

The equilibrium gradient is dependent on rotor speed, temperature, and on the molecular weight and buoyancy of the solute. This equation can be fitted by nonlinear least squares.

$$\omega^2 r c \frac{M(1-\bar{v}\rho)}{N_0 f} = \frac{kT}{f} \left(\frac{dc}{dr} \right) \implies \omega^2 r c M(1-\bar{v}\rho) = N_0 kT \left(\frac{dc}{dr} \right)$$

Separate the variables and integrate the differential equation over r_0 to r and from c_0 to c_r :

$$M(1-\bar{v}\rho)\omega^2 \int_{r_0}^r r dr = RT \int_{c_0}^{c_r} \frac{1}{c} dc \implies M(1-\bar{v}\rho)\omega^2 \frac{1}{2}(r^2 - r_0^2) = RT \ln \frac{c_r}{c_0}$$

$$\implies \ln c_r = \frac{M(1-\bar{v}\rho)\omega^2}{2RT} r^2 - \frac{M(1-\bar{v}\rho)\omega^2}{2RT} r_0^2 + \ln c_0$$

This equation has the form of the equation of a straight line, $y = mx + b$, where $\ln c_r = y$ and $r^2 = x$. If we plot $\ln c_r$ vs. r^2 , the result should be a straight line with a slope = $\frac{M(1-\bar{v}\rho)\omega^2}{2RT}$. Concentration, c , can be measured at each radius, r , using optical systems built into analytical ultracentrifuges.

